## Uplink Design

$$\left(\frac{C}{N_0}\right)_{uplink \text{ in db Hz}} = 10\log P_T G_T - 20Log\left(\frac{4\pi d}{\lambda}\right) + 10\log\frac{G}{T}$$
$$-10LogL_A - 10LogK - BO_i$$

#### COMPLETE LINK DESIGN

- TWO EARTH STATION AND SATELLITE
- UP LINK AND DOWN LINK
- (UPLINK,SATELLITE TRANSPONDER, DOWN LINK
- UPLINK (C/No)u AT TRANSPONDER INPUT
- DOWNLINK (C/No)d

### Complete link design cont---

$$C = \frac{C_U G_s G_T G_R}{L}$$

C - Carrier Signal At Receiving Earth Station
CU - SIGNAL POWER AT THE SATELLITE TRANSPONDER
INPUT

Gs – SATELLITE TRANSPONDER GAIN

GT- GAIN OF THE SATELLITE TRANSMITTING ANTENNA

GR – GAIN OF THE RECEIVING ANTENNA

L – LOSSES ON THE DOWN LINK

# NOISE POWER SPECTRAL DENSITY AT THE INPUT OF THE RECEIVING ANTENNA

$$N_0 = N_{0D} + \frac{N_{0U}G_sG_TG_R}{L}$$

N₀ IS NOISE POWER SPECTRAL DENSITY AT THE INPUT OF THE RECEIVING STATION

Nou IS NOISE POWER SPECTRAL DENSITY AT THE TRANSPONDER INPUT

$$\frac{C}{N_{0}} = \frac{\frac{C_{U}G_{s}G_{T}G_{R}}{L}}{N_{0D} + \frac{N_{0U}G_{s}G_{T}G_{R}}{L}}$$

$$= \frac{C_{U}G_{s}G_{T}G_{R}}{N_{0U} + \frac{N_{0D}L}{G_{s}G_{T}G_{R}}}$$

TRANSPONDER HAS A BAND WIDTH B AND RADIATES A CONSTANT POWER  $P_{\mathsf{T}}$  AND ITS GAIN  $G_{\mathsf{S}}$ 

$$G_S = \frac{P_T}{C_U + N_{OU} * B}$$

#### FOR DOWN LINK SIGNAL POWER CD

$$C_D = \frac{P_T G_T G_R}{L}$$

THUS C/No

$$\frac{C}{N_{0}} = \frac{C_{U}}{N_{0U} + \frac{N_{0D}.L(C_{U} + N_{0U} * B)}{P_{T}.G_{T}G_{R}}}$$

$$= \frac{C_{U}}{N_{0U} + \frac{N_{0D}.(C_{U} + N_{0U} * B)}{C_{D}}}$$

$$\frac{C}{N_{0}} = \frac{\frac{C_{U} * C_{D}}{N_{0U} * N_{0D}}}{\frac{N_{0U} * C_{D} + N_{0D} \cdot (C_{U} + N_{0U} * B)}{N_{0U} * N_{0D}}}$$

$$= \frac{\left(\frac{C}{N_{0}}\right)_{u} * \left(\frac{C}{N_{0}}\right)_{D}}{\left(\frac{C}{N_{0}}\right)_{u} + \left(\frac{C}{N_{0}}\right)_{D}} + B$$

$$\left(\frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} \to B \le \left(\frac{C}{N_{0}}\right) & & & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} \to B \le \left(\frac{C}{N_{0}}\right) & & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} \to B \le \left(\frac{C}{N_{0}}\right) & & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} \to B \le \left(\frac{C}{N_{0}}\right) & & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} \to B \le \left(\frac{C}{N_{0}}\right)^{-1} & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} & & & \\ \frac{C}{N_{0}}\right)^{-1} & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} & & \\ \frac{C}{N_{0}}\right)^{-1} & & & \\ \frac{C}{N_{0}}\right)^{-1} = \left(\frac{C}{N_{0}}\right)^{-1} + \left(\frac{C}{N_{0}}\right)^{-1} & & \\ \frac{C}{N_{0}}\right)^{-1} & & & \\ \frac{C}{N_{0}}\right)^{-1} & \\ \frac{C}{N_{0}}\left(\frac{C}{N_{0}}\right)^{-1} & & \\ \frac{C}{N_{0}}\right)^{-1} & & \\$$

## Complete link design

- Effect of interfering signals
- I is noise power involved with the interfering signals under the band width of the desired carrier than, the net C/N ratio (for uplink)

$$\left(\frac{C}{N}\right)_{netuplink} = \left[\left(\frac{C}{N}\right)_{U}^{-1} + \left(\frac{C}{I}\right)_{U}^{-1}\right]$$

$$\left(\frac{C}{N}\right)_{net\ downlink} = \left[\left(\frac{C}{N}\right)_{D}^{-1} + \left(\frac{C}{I}\right)_{D}^{-1}\right]^{-1} \\
\left(\frac{C}{N}\right)_{net} = \left[\left(\frac{C}{N}\right)_{Net\ uplink} + \left(\frac{C}{N}\right)_{net\ downlink}\right]^{-1} \\
= \left[\left(\frac{C}{N}\right)_{u}^{-1} + \left(\frac{C}{I}\right)_{u}^{-1} + \left(\frac{C}{N}\right)_{D}^{-1} + \left(\frac{C}{I}\right)_{D}^{-1}\right]^{-1} \\
\left[\left(\frac{C}{N}\right)^{-1} + \left(\frac{C}{I}\right)^{-1}\right]^{-1} \\
\left(\frac{C}{N}\right)^{-1} = \left(\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} \\
\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} \\
\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} \\
\frac{C}{N}\right)^{-1} + \left(\frac{C}{N}\right)^{-1} + \left(\frac$$

### Complete link design contt---

- C/N CARRIER TO NOISE OF OVERALL LINK
- C/I CARRIER TO INTERFACE RATIO OF OVERALL LINK
- C/I > C/N SATELLITE LINK IS NOISE DOMINANT
- C/I< C/N SATELLITE IS CALLED INTERFERANCE DOMINENT
- FOR A TYPICAL FM DEMODULATOR S/N AFTER DEMODULATOR
- (S/N)<sub>OUTPUT</sub> = (C/N)<sub>in</sub> +FM <sub>IMPROVEMENT</sub>

### Earth station parameter

$$\frac{C}{N_0} = \frac{P_T G_T G_R}{KT_S} \left(\frac{\lambda}{4\pi d}\right)^2 \frac{1}{L_A}$$

 d is the range between transmitting and receiving antenna

$$G = \eta \left(\frac{4 \pi D}{\lambda}\right)^{2}$$

$$G = \frac{\eta 4 \pi^{2} 70^{2}}{\theta^{2} dR}$$

#### Contd---

- η antenna efficiency
- (θ3db) sat satellite antenna beam width
- Des is earth station diameter

$$G = \eta \left(\frac{4 \pi D}{\lambda}\right)^{2}$$

$$G = \frac{\eta 4 \pi^{2} 70^{2}}{\theta^{2} dR}$$

### Earth station parameter

$$\frac{C}{N_0} = \frac{P_T}{L_A N_0} \eta_T \eta_R - \frac{\pi^2 70^2 D_{ES}^2}{d^2 (\theta_{3db})_{sat}^2}$$

#### FOR FIXED EARTH STATION

$$\frac{C}{N_0} = \frac{P_T}{L_A N_0} \eta_T \eta_R \frac{\pi^2 C^2 70^2}{(4d)^2 (\theta_{3db})_{sat}^2 (\theta_{3db})_{ES}^2 \cdot f^2}$$

$$\frac{C}{N_0} = \frac{P_T}{L_A N_0} \eta_T \eta_R \left( \frac{\pi D_{sat} D_{ES}}{4 dC} \right)^2 f^2$$

### Assignment 6

 Derive the expression for C/N ratio of satelite link design.